

Rijksdienst voor Ondernemend Nederland

Morphodynamics of Borssele Wind Farm Zone

Sites I and II commissioned by RVO

Tim Raaijmakers Hendrik Jan Riezebos Thaiënne van Dijk Tommer Vermaas Bas Borsje Robert Hasselaar

Webinar 20 October 2015



Deltares

Enabling Delta Life

Introduction to morphodynamics team @ webina

Presenter:

Tim Raaijmakers

Senior researcher/advisor, Programme Manager Offshore Engineering, Project Leader Morphodynamics study

Moderators:

Hendrik Jan Riezebos

Researcher/advisor Offshore Engineering and co-author of Morphodynamics report

Thaiënne van Dijk

Specialist Marine Geology at Deltares, Assistant Professor in Marine Systems at the University of Twente

Frank van Erp

Senior advisor Renewable Energy - RVO









Goal: to determine design seabed levels resulting from autonomous morphodynamical processes for Borssele Wind Farm Zone in period 2015-2046

Deltares

Phase I: Desk study morphodynamics for entire Borssele Wind Farm Zone

- Based on in-house bathymetrical data (most recent: 2010)
- Delivery date of report: <u>December 2014</u>

Phase IIa: update of desk study for BWFS-I and II

- Extension based on additional survey by Deep of BWFS I and II
- Delivery date of report: <u>June 2015</u>
- Topic of today's webinar

Phase IIb: update of desk study for BWFS-III and IV

- Extension based on additional survey by Fugro of BWFS III and IV
- Will be based on new site contours (including Site V)
- Delivery date of report: <u>November 2015</u>

Contents of presentation

- Introduction Deltares
- Introduction Morphodynamics
- Methodology of this study
- Results
- Conclusions and Recommendations





Introduction to Deltares

Deltares is an **independent** institute for **applied research** in the field of **water, subsurface and infrastructure**.

- merger since 2008 of WL | Delft Hydraulics, GeoDelft and parts of TNO and Rijkswaterstaat
- applied research & specialist consultancy
- independent: serving companies and governments
- extensive hydraulic/geotechnical laboratories and computer modelling facilities
- active in research networks: JIP, EU, FLOW, TKI,...
- open-source policy: "dare to share"
- > > 800 staff (mostly MSc/PhD), > 28 nationalities
- main offices in Delft and Utrecht, The Netherlands
- branch offices in Singapore, USA, Jakarta,
 Abu Dhabi/Dubai, Rio de Janeiro







Deltares' activities in offshore wind

Hydrodynamics

- Metocean/environmental conditions (waves, currents, water levels)
- ✓ Operational forecasting systems (for installation and O&M)
- ✓ Wave loads / impacts on foundations

Geotechnics

- ✓ Geotechnical design of foundations (e.g. cyclic liquefaction)
- Pile installation techniques (impact-driving, vibrating)
- ✓ Cable burial techniques (jetting, ploughing, trenching, self-burial)
- External threats to electricity cables (anchors, fishnets, objects)







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Morphology & morphodynamics

- Offshore geology, seabed characteristics
- Scour and scour protection for all kinds of foundations
- Bed level changes due to morphodynamics (e.g. sand waves)
- ✓ Cable routing and site selection in morphodynamic areas

Offshore surveying

Seismic, sonar and other hydrographic surveys







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"*Morphodynamics*, the study of landscape changes due to erosion and sedimentation" [wiktionary]

"Morphodynamics refers to the study of the interaction and adjustment of the seafloor topography and fluid hydrodynamic processes, seafloor morphologies and sequences of change dynamics involving the motion of sediment. Hydrodynamic processes include those of waves, tides and wind-induced currents." [wikipedia]



Seabed Morphodynamics

Distinguish between hydrodynamic driving forces:

- Coastal profile: often (storm) wave-driven
- Estuaries with tidal channels and flats
- Offshore seabed with sand banks, sand waves, megaripples etc.

The export cable crosses all area types: requires combination of numerical modelling of storm events (e.g. XBeach, UNIBEST), tidal climate (e.g. Delft-3D) and data-driven methods.



<u>Link</u>





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Sand Wave Morphodynamics

- Inherent property of sandy seabeds
- Development due to tidally averaged recirculation cells
- Global phenomenon of sandy beds in shallow seas !
- Sand wave length: typically 200-600 meters
- Sand wave height: 10-30% of the water depth
- Migration Rate: up to 10s of meters per year





Sand Wave Morphodynamics – Analysis techniques

Two methods to investigate sand wave characteristics:

- 1. Data-driven analysis based on seabed surveys
 - Preferably 3 (or more) good quality surveys
 - Preferable covering a time span of 10 years (or more)
- 2. Numerical modelling
 - Using a process-based morphological model (e.g. Delft3D)
 - Driven by detailed tidal climate boundary conditions



Sand Wave Morphodynamics – Analysis techniques

Two methods to investigate sand wave characteristics:

1. Data-driven analysis based on seabed surveys

Most reliable, if data is available

2. Numerical modelling

Only option, if limited/no data is available; useful to investigate dependencies on governing parameters



Example of Sand Wave Model in Delft-3D



Self-organizing of random bed perturbations into natural sand wave fields that correspond to the local hydrodynamic forcing, water depth and seabed material



3D-Sand Wave Model in Delft-3D

t = 0: Random bed perturbations and chaotic velocity field



Sand waves and their environmental dependencies

Migration Rate:

- Grain size
- Tidal asymmetry
- > Wavelength

Amplitude:

- Grain size
- Tidal asymmetry
- Peak tidal velocity
- Water depth

Wavelength:

- Grain size
- Peak tidal velocity



Migration rate vs. tidal asymmetry

Rel. wave height vs. peak tidal velocity

Sand wavelength vs. grain size



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Required Design Seabed Levels

Reference SeaBed Level (RSBL)

The lowest possible seabed level in the period 2015-2046 RSBL = Static Seabed Level - Max. Negative Envelope of Sand Wave Field until 2046 + Uncertainty Band

Maximum SeaBed Level (MSBL)

The highest possible seabed level during the lifetime of the wind parks MSBL = Static Seabed Level + Max. Positive Envelope of Sand Wave Field until 2046 + Uncertainty Band



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Maximum seabed lowering in period 2015-2046

Difference between 2015-bathymetry and RSBL

Maximum seabed rising in period 2015-2046 Difference between 2015-bathymetry and MSBL



Methodology and calculation steps (I)

In order to predict these levels for the BWFZ, the following techniques were used:

- 1. Obtaining 3 bathymetrical datasets
- 2. Large-scale bathymetric filtering to distinguish between the "static" and "mobile" seabed features
- 3. Filtering and analysis of megaripples (to be part of the uncertainty band)
- 4. Extraction of the sand wave field (excluding sand banks and megaripples) for sand wave analysis
- 5. Automated detection of sand wave migration directions
- 6. Fourier analysis on individual sand waves to determine sand wave migration rates



latitude [°N]

Methodology and calculation steps (II)

- Estimating uncertainty range based on measurement errors, processing inaccuracies and smaller scale seabed features such as megaripples
- 8. Migration of sand wave fields with calculated migration rates and directions
- 9. Combining migrated sand wave fields with "static" bathymetry and uncertainty range to compute RSBL and MSBL
- 10. Comparing the isopach of the base of the Holocene Formation with the RSBL to avoid overly conservative downward bed level changes
- 11. Translate RSBL and MSBL into zones with various recommendation levels for offshore foundations and cables



Definitions of various bathymetrical data sets used in this study

Short name	Description	Sand banks	Sand waves	Mega- ripples
2015 bathymetry	Full measured bathymetry by Deep in 2015	X	Х	Х
Static bathymetry	Long-term mean bathymetry (for the considered period / lifetime of wind farms)	X		
Quasi-static bathymetry	Bathymetry with megaripples filtered out	X	Х	
Mobile bathymetry	Bathymetry with mobile morph. seabed features (sand wave directions + Fourier analysis)		Х	X
Sand Wave field	Sand wave field without megaripples (to migrate future bathymetries, RSBL, MSBL)		Х	
Megaripple field	Megaripple field (to determine uncertainty band)			X

Methodology – Bathymetry 1999/2000/2001

Bathymetry constructed of 4 SBES in 1999, 2000 and 2001, taken by the Netherlands Hydrographic Office of the Royal Netherlands Navy.

(note the site contours have changed in the meantime and Site V has been added in the northern part of Site III)



Methodology – Bathymetry 2010

Bathymetry constructed of 3 MBES in 2010, taken by the Netherlands Hydrographic Office of the Royal Netherlands Navy.

(note the site contours have changed in the meantime and Site V has been added in the northern part of Site III)



Methodology – Bathymetry 2015



- Deep (Site I and II)
- ➢ Fugro (Site III and IV)

(note the site contours have changed in the meantime and Site V has been added in the northern part of Site III)



Methodology – Large-scale bathymetric filtering



- Goal is to separate mobile and static bathymetry
- Sand waves have an average crest orientation around the SE-NW-axis and the sand banks have an average orientation more or less perpendicular to the sand waves
- For filtering it was decided to use an **ellipsoid** with the long axis under an angle of **45°N**. The filter size along the long axis was chosen at **1000m**, while the filter size along the short axis was only **50m**.
- In this way, averaging over the sand waves did not cause too much smoothening of the sand banks, while a filter size of 1000m is longer than the longest observed sand wave lengths in the BWFZ, ensuring that all sand waves are filtered out



static bathymetry







-35

-30

-20

-15

Mobile bathymetry in 2000



mobile bathymetry

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-20

-15

static bathymetry



-20

-15

= mobile bathymetry



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-25

-20

-15





long-term mean seabed level rel, to LAT [m]

-20

-15





Methodology – Check difference between static bathies

If the filtering method is accurate and if the Static Bathymetries are indeed "static", the differences between different years should be negligible:



- Differences are minor: but no migration or growing/shrinking of sand banks can be observed.
- Assumption of static sand banks over periods of decades seems valid.

Methodology – megaripple analysis (I)

- megaripples have large migration speeds: many megaripples will pass at each foundation throughout the lifetime of wind farms.
- > the migration of the megaripples will and cannot be determined from the data
- solution: analyse the megaripple field and include some representative statistical values in the uncertainty band



- bathymetry filtered with block filter of 15m to obtain "Sand Wave Field"
- 2015-survey (1x1m) used for analysis
- rather irregular megaripple pattern



Methodology – megaripple analysis (II)

- Megaripple field analyzed to determine trough depths and crest heights
- Non-exceedance curves determined for WFS-I and WFS-II
- The 95% nonexceedance values:
 ~0.40m: trough depth
 ~0.60m: crest height
- These values will be included as uncertainty



Methodology – Direction of sand wave migration

- Analyze sand wave fields at many different transects
- Determine migration directions by finding the best fit (optimizing cost function)
- Directions determined for 3 combinations of differences between Mobile Bathymetries for 665 random transects:
 - ✓ 2010 2000
 - ✓ 2015 2000
 - ✓ 2015 2010



purple transects: migration to NE black transects: migration to SW



Methodology – Direction of sand wave migration

- The sand waves in the BWFZ are migrating to the southwest (ebb direction) as well as to the northeast (flood direction)
- With a main axis of approximately 230°N and 50°N. This axis varies over the area with a variation of up to 30°



Methodology - Fourier analysis on transects

- Identify crests and troughs
- Track identified points
- Obtain statistics per transect
- Some manual steps:
 - Check each transect
 - Generation / extinction of small waves / megaripples
- Sand wave statistics are determined by combining results for each transect and 3 survey combinations (2000/2010, 2000/2015, 2010/2015)



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Results – Sand Wave Statistics

- Non-exceedance curves for migration rate are determined per transect and for each of the three bathymetry-combinations
- 10%-value represents the conservative most NEdirected migration rate
- 50%-value represents the best estimate migration rate
- 90%-value represents the conservative most SWdirected migration rate
- Note that the actual directions are taken into account instead of SW/NE





Results – sand wave statistics WFS-I

Exceedance curves for 2010/2015



migration distance total [m]



positive is towards SW; negative towards NE **Deltares**

Results – sand wave statistics WFS-II

Exceedance curves for 2010/2015 (positive is towards SW; negative towards NE)

Sand wave statistics for WFS-I

Parameter	10% non- exceedance (2010/2015)	50% non- exceedance (2010/2015)	90% non- exceedance (2010/2015)	
Migration distance [m]	-8	-2	7	
Migration speed [m/yr]	-1.7	-0.4	1.5	
Wave length [m]	141/133	236/228	391/387	
Wave height [m]	2.1/2	3.9/3.9	5.7/5.9	

Sand wave statistics for WFS-II

Parameter	10% non- exceedance (2010-2015)	50% non- exceedance (2010-2015)	90% non- exceedance (2010-2015)
Migration distance [m]	-8	1	10
Migration speed [m/yr]	-1.7	0.2	2.1
Wave length [m]	124/122	241/242	455/450
Wave height [m]	1.5/1.6	3.2/3.3	5.7/5.7

Results – dealing with uncertainty

Several sources of uncertainty:

- I. Uncertainty due to data collection and differences in the collection of data (e.g. SBES (shoal-biased, lower density) vs. more accurate MBES)
- II. Uncertainty in the pre-processing of data
 - (e.g. vessel movements, tidal reduction, gridding)
- III. Uncertainty in the methodology of analysis and prediction
 - (e.g. assumption of shape-retaining sand waves, megaripple migration)

Uncertainty band in this study consists of contributions related to:

- survey inaccuracies
- existence of megaripples

survey uncertainty (95%)	= 0.20m
megaripple uncertainty (95%)	= 0.60m
uncertainty upward	= 0.80m
survey uncertainty (95%)	= -0.20m
survey uncertainty (95%) megaripple uncertainty (95%)	= -0.20m = -0.40m

Results – predicting future bathymetries until 2046

- In total, 9 estimates for the migrated sand wave field are determined for each year in the period 2015-2046
- These 9 estimates consist of 3 sand wave migration directions (2000/2010, 2000/2015, 2010/2015) times 3 estimates for the migration rate (10%, 50% and 90% determined from sand wave statistics)
- Predicted bathymetries for year 20XX are reconstructed by combining:
 - ✓ Static Bathymetry 2015
 - ✓ Migrated Sand Wave Field 2015 until year 20XX
 - ✓ Uncertainty Band

Movie illustarting seabed predictions (300yr!) for one out of nine maps of migration directions and migration rates

Results – 1/9 predicted bathymetry in 2046

(1/9) migrated sand wave fields

(1/9) bathymetries 2046

Results – determining RSBL

Reference SeaBed Level The lowest possible seabed level during the lifetime of the wind parks

RSBL = Static Seabed Level - Max. Negative Envelope of Sand Wave Field until 2046 -Uncertainty Band

The RSBL varies between -16.1m and -40.3m LAT

Results – Maximum Potential Seabed Lowering

Difference between 2015-bathymetry and RSBL

Results – determining MSBL

Maximum SeaBed Level The highest possible seabed level during the lifetime of the wind parks

MSBL = Static Seabed Level + Max. Positive Envelope of Sand Wave Field until 2046 + Uncertainty Band

The MSBL varies between -13.3m and -38.2m LAT

Results – Maximum Potential Seabed Level Rise

Difference between 2015-bathymetry and MSBL

Results – Maximum Potential Seabed Level Rise

Results – comparing RSBL with MSBL

Maximum vertical range in (autonomous) morphological seabed changes

Classification zones

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- Next step: translate MSBL and RSBL and corresponding seabed changes to "Classification Zones"
- Classification chosen less strict for rising seabed levels. The reasoning behind this is that close to the structures, local scour will counteract rising seabed levels. This does not apply to the electricity cables, which are buried in the seabed; rising seabed levels can be of influence on the maximum cable temperature.

Classification of zones	Bed level lowering [m]	Bed level rising [m]		
Preferred	0 > dz ≥ -1	$0 < dz \le 2$		
Possible	-1 > dz ≥ -2	$2 < dz \le 3$		
Better avoided	-2 > dz ≥ -3	$3 < dz \le 5$		
Unrecommended	dz < -3	dz > 5		

Classification Zones are for indicative and illustrational purposes only. Actual classification is dependent on the design of the support structures and properties of electricity cables and should be adjusted accordingly once this information is available.

Classification zones: example for one transec

Example for one transect:

- Classification calculated for both rising and lowering seabed
- Most strict classification (rising/lowering) is used

Classification zones for southern part Site

Classification zones for Site I and II

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Conclusions (I)

- The bathymetry in BWFZ consists of a complex system of shore-parallel sand banks covered with shore-perpendicular sand waves; covered with highly mobile megaripples.
- The sand banks are considered to be static over the lifetime of the wind parks to be developed in the area (negligible change observed in 15 years).
- The sand waves are (mostly) mobile, have an average length of 230m, average height of 4m and typical migration speeds are in the order of -1.7m/yr (governing NE-direction) to 2.1 m/yr (governing SW-direction).

Area	Wave height 50% non- exceedance [m] (2010/2015)	Wavelength 50% non- exceedance [m] (2010/2015)	Migration speed 10% non- exceedance [m/yr]	Migration speed 90% non- exceedance [m/yr]
WFS-I	3.9/3.9	236/228	-1.7	1.5
WFS-II	3.2/3.3	241/242	-1.7	2.1
WFS-I and II combined	3.6/3.7	239/236	-1.7	1.9

Megaripples are very mobile, but limited in height: therefore they are added as an uncertainty band on top of the predictions
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Conclusions (II)

- Seabed changes are predicted for a range of predictions of sand wave migration (3 migration directions x 3 migration speeds)
- Maximum SeaBed Level (MSBL) and Reference SeaBed Level (RSBL) are determined.
- This results in maximum potential seabed lowering and rising until 2046
- Classification Zones (preferred / possible / better avoided / unrecommended) are determined based on estimated ranges for downward and upward seabed changes

Recommendations for design

- 0313 C
- A. Further improve accuracy of morphodynamic predictions:
- Set up a detailed hydrodynamic model of the area and simulate the tidal currents to assess tide-averaged sediment transport rates.
- In case of an additional pre-installation survey (~2018): re-run analysis and further narrow down uncertainty ranges, which will be beneficial for scour mitigation strategy and/or cable burial depth
- **B.** Include morphodynamic activity in wind farm design:
- Take predicted morphodynamic seabed changes into account in determining WTG-locations and cable trajectories
- Consider morphodynamic changes in combination with scour mitigation strategy
- Deploy continuous cable burial depth monitoring system coupled with morphodynamic prediction model to guarantee cable safety

Thank you for your attention!

¿Questions?

Scale model in Deltares' Atlantic Basin of Dolwin-2 transformer platform located in German Bight (North Sea)

More information? Email: tim.raaijmakers@deltares.nl